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AFDELING TOEGEPASTE WISKUNDE

Technical Note TN 23

A note on the effect of a return surge

by

H.A. Lauwerier

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The object of this note is to show the effect of a "return surge" on the elevation of the North Sea by means of a mathematical model. The geometry of the model is determined by the rectangle  $0 < x < a$ ,  $0 < y < b$ , where  $x=0$ ,  $x=a$ ,  $y=0$  represent coasts and  $y=b$  the open end at the ocean. The depth  $h$  is given by the exponential function

$$(1) \quad h = h_0 e^{\beta y}.$$

The numerical values are  $a=400$  km,  $b=800$  km,  $h_0=33$  m,  $h(b)=158$  m.

The hydrodynamical equations are

$$(2) \quad \begin{cases} (\frac{\partial}{\partial t} + \lambda)u - \Omega v + gh \frac{\partial \eta}{\partial x} = U \\ (\frac{\partial}{\partial t} + \lambda)v + \Omega u + gh \frac{\partial \eta}{\partial y} = V \\ \frac{\partial \eta}{\partial t} + \frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0, \end{cases}$$

with the boundary conditions

$$(3) \quad \begin{cases} u=0 & \text{for } x=0, \quad x=a \\ v=0 & \text{for } y=0 \\ \eta=0 & \text{for } y=b \end{cases},$$

and with the initial condition

$$(4) \quad u=v=\eta=0 \quad \text{for } t=0.$$

The numerical values of the coefficients of friction and rotation are  $\lambda=0.09 \text{ hr}^{-1}$ ,  $\Omega=0.44 \text{ hr}^{-1}$ .

A numerical calculation has been carried out by means of a difference scheme for the particular windfield

$$(5) \quad \begin{cases} v = \begin{cases} -\sin \frac{\pi c t}{10 a} & \text{for } 0 \leq t \leq \frac{10 a}{c} \\ 0 & \text{for } t > \frac{10 a}{c} \end{cases} \end{cases} \quad U=0$$

where  $c$  denotes the mean velocity of free waves, numerically  $c=91$  km/hr. This windfield represents a uniform "Northern" wind varying sinusoidally with a duration of 44 hr (see fig.1).

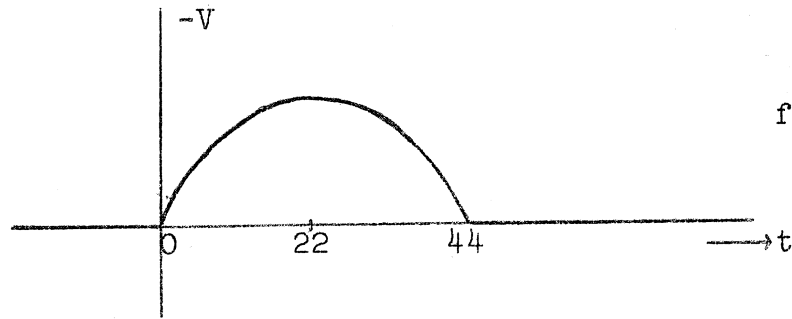


figure 1

Computations have been carried out for a grid with a basic mesh of  $\delta = a/24$ , i.e. with squares of  $16 \times 16$  km. The elevations were calculated at all points  $x = (2m+1)\delta$ ,  $y = (2n+1)\delta$  with  $m=0,1,\dots,11$ ,  $n=0,1,\dots,23$ . The following table gives the elevations at the points indicated by small circles in figure 2 at intervals of  $2\tau$  or  $3\tau$  where  $\tau = \frac{a}{\pi c} = 1.4$  hour. The elevations are given in centimeters.

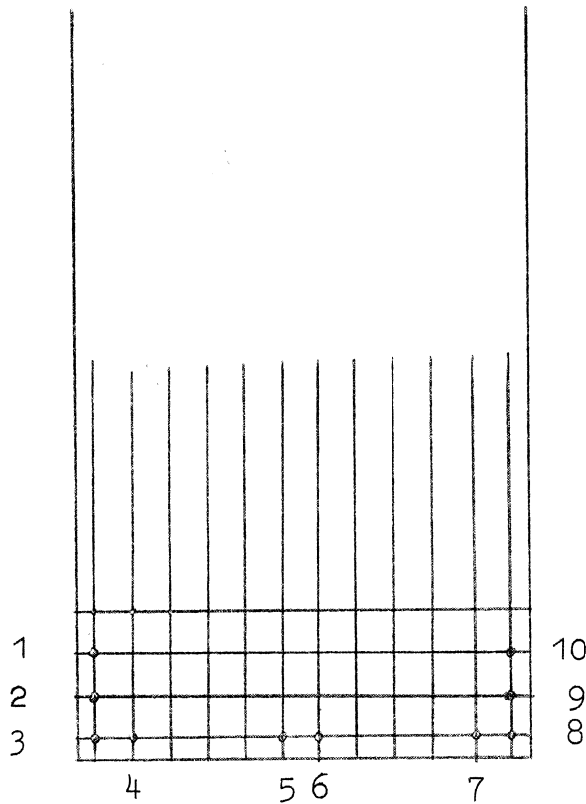


figure 2

Situation of points nos 1, ..., 10.

point no time	1	2	3	4	5	6	7	8	9	10
2 $\tau$	14	19	26	24	22	22	20	19	10	3
4 $\tau$	82	92	107	102	79	75	63	61	42	25
6 $\tau$	182	200	224	215	172	160	125	121	93	68
9 $\tau$	337	367	404	394	353	342	305	301	256	214
12 $\tau$	469	510	556	547	509	498	464	463	410	362
15 $\tau$	532	577	627	622	605	601	586	587	531	478
18 $\tau$	544	592	642	639	634	632	628	631	578	529
21 $\tau$	499	541	585	586	597	600	611	615	570	528
24 $\tau$	418	454	489	493	514	519	537	541	508	477
27 $\tau$	298	322	345	352	385	393	421	425	406	389
30 $\tau$	156	168	177	186	225	235	267	271	269	266
33 $\tau$	4	6	5	15	59	71	107	109	117	124
36 $\tau$	-50	-53	-57	-52	-38	-33	-15	-14	-6	1
38 $\tau$	-47	-49	-53	-51	-52	-53	-57	-60	-53	-47
40 $\tau$	-31	-34	-36	-35	-36	-37	-44	-47	-44	-42
42 $\tau$	-7	-9	-11	-11	-19	-21	-28	-31	-28	-27
44 $\tau$	8	8	8	8	2	0	-10	-12	-11	-11
46 $\tau$	9	8	8	8	11	11	10	9	9	8
48 $\tau$	12	12	12	12	11	11	13	12	13	14
50 $\tau$	7	8	9	9	11	12	11	11	11	12

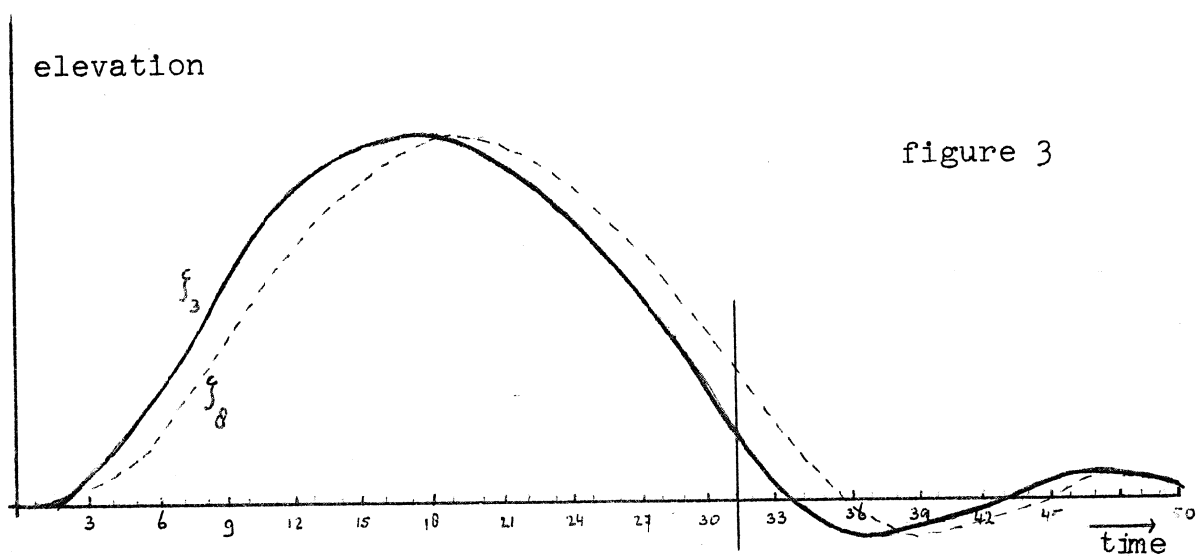


figure 3

Elevation at the points no 3 and 8 from the above table

Similar calculations have been carried out for the windfield

$$(6) \quad \begin{cases} U = 0 \\ V = \begin{cases} -1 & \text{for } t < 0 \\ 0 & \text{for } t > 0 \end{cases} \end{cases}$$

This windfield represents a uniform and constant "Northern" wind which stops suddenly at  $t=0$ .

At that time the sea is in its equilibrium position

$$(7) \quad u=v=0, \quad gh_0 \zeta = \frac{e^{-\beta y} - e^{-\beta b}}{\beta}$$

The following table shows that the subsequent motion has the appearance of a strongly damped oscillation.

point no time	1	2	3	4	5	6	7	8	9	10
0	510	555	603	603	603	603	603	603	556	511
$3\tau$	167	184	192	210	312	339	383	387	391	396
$6\tau$	-44	-47	-52	-45	16	45	142	150	165	178
$9\tau$	-112	-112	-113	-107	-84	-82	-105	-120	-108	-94
$12\tau$	-63	-80	-90	-89	-108	-113	-99	-95	-83	-72
$15\tau$	-8	-5	-1	5	9	1	-26	-30	-40	-45
$18\tau$	30	27	29	23	4	1	14	16	17	22
$21\tau$	9	11	12	14	23	22	21	21	21	20
$24\tau$	11	15	17	17	15	18	19	19	22	24
$27\tau$	-14	-10	-5	-4	1	-1	-13	-14	-12	-8
$30\tau$	-3	-1	1	1	-1	0	9	10	8	7

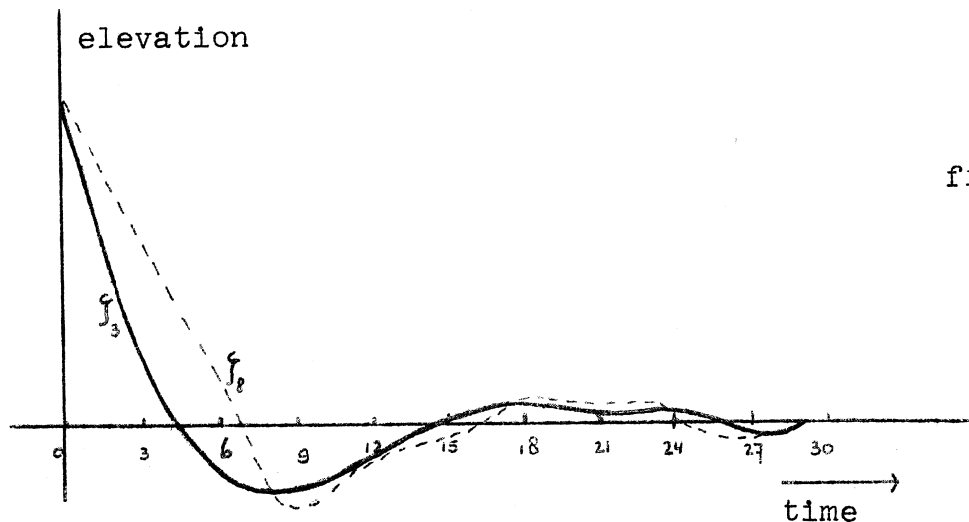


figure 4

Elevation at the points 3 and 8 from the above table.

These two cases indicate that any disturbance of the elevation is damped out very rapidly.

Considering figure 3 first, we see that after the wind has stopped the elevation has a negative extremum which is about 10% of the previous maximum.

If all signs are inverted we obtain the following conclusion.

A uniform sinusoidal "Southern" wind of the type (5) brings about a low water followed by a high water (return surge) the intensity of which is of the order of 10% of the previous low tide.

Considering next figure 4 we arrive at a similar conclusion:

If a uniform and constant "Southern" wind blows sufficiently long as to bring the sea in its equilibrium position and then suddenly stops, then after an interval of 12 to 15 hours a return surge develops, the intensity of which is of the order of 20% of the previous minimum.

Finally an illustrative numerical example will be given. For a uniform "Southern" wind of the type (5) with a maximum of 30 m/sec a return surge of about 0.33 m. is obtained after an initial low water of about -3.40 m. For a uniform and constant "Southern" wind of 30 m/sec a return surge of about

0.60 m. is obtained after an initial low water of about -3.20 m.

### References

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